

UNIVERSITY OF NOTRE DAME  
Aerospace and Mechanical Engineering

**ME 469: Introduction to Robotics**  
**Homework 3 Solutions**

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1. (Craig, 3.16)

The link frame assignments are illustrated in Figure 1 (any axis not shown is determined by the right hand rule).

Consulting the figure, and naming the distances  $a_1$  and  $a_2$ , the following link parameters are apparent:

| $i$ | $\alpha_{i-1}$  | $a_{i-1}$ | $d_i$       | $\theta_i$ |
|-----|-----------------|-----------|-------------|------------|
| 1   | 0               | 0         | 0           | $\theta_1$ |
| 2   | $\frac{\pi}{2}$ | $a_1$     | $d_2 + a_2$ | 0          |
| 3   | $\frac{\pi}{2}$ | 0         | 0           | $\theta_3$ |

Note that I took the the reference value for  $\theta_3$  to be the position of the wrist when it is “straight out,” and the reference value for  $d_2$  to be zero when the frame 3 is located a distance of  $a_2$  away from frame 2.

Plugging into Equation 3.6, or the Mathematica function gives the forward kinematics

$${}^0_3T = \begin{bmatrix} \cos(\theta_3 - \theta_1) & -\sin(\theta_3 - \theta_1) & 0 & a_1 \cos(\theta_1) + (d_2 + a_2) \sin(\theta_1) \\ -\sin(\theta_3 - \theta_1) & -\cos(\theta_3 - \theta_1) & 0 & -((d_2 + a_2) \cos(\theta_1)) + a_1 \sin(\theta_1) \\ 0 & 0 & -1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

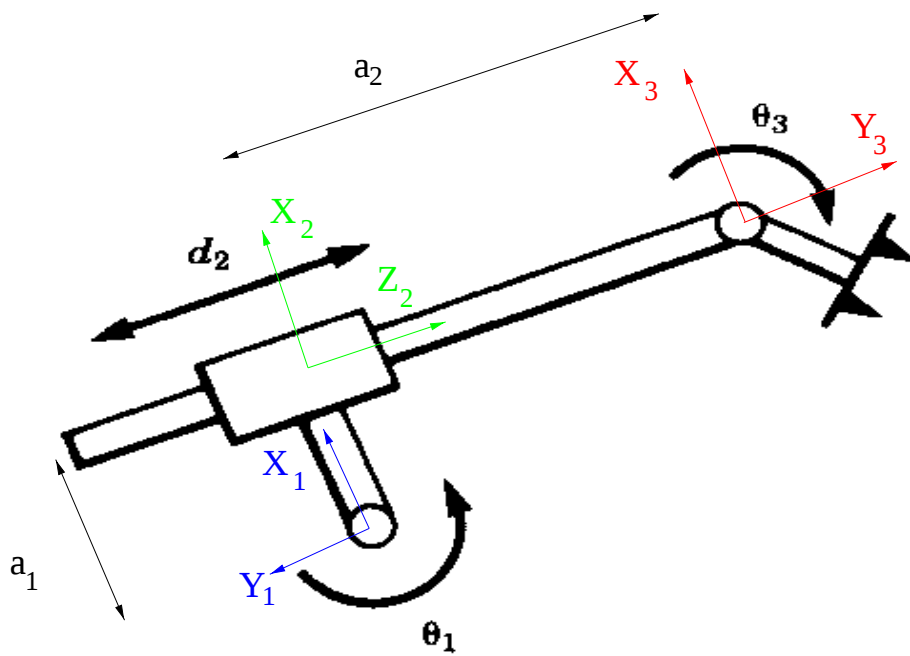
2. (Craig, 3.19)

For this problem, take the zero position of the links as follows:

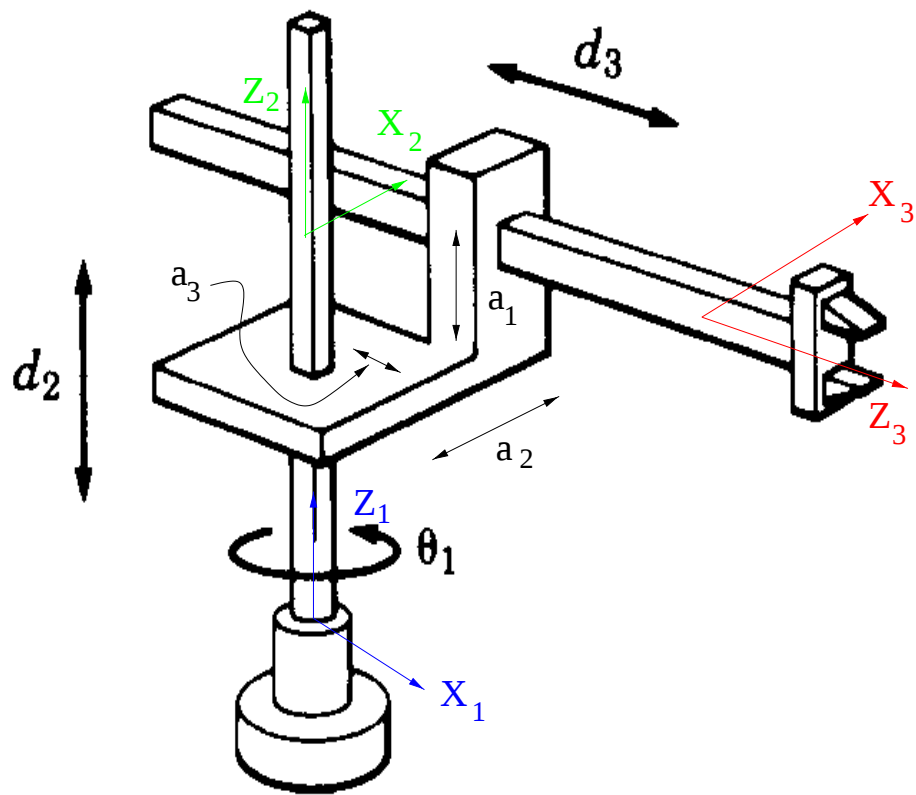
- for link 2, let  $d_2 = 0$  when the link is all the way “down” and
- for link 3, let  $d_3 = 0$  when the wrist is flush against the joint stop, *i.e.*, all the way to the left.

The link frame assignments are illustrated in Figure 2.

Consulting the figure and naming the distance  $a_2$ , the following link parameters are apparent:



**Figure 1.** Link frame assignments for problem 1.



**Figure 2.** Link frame assignments for problem 2.

| $i$ | $\alpha_{i-1}$  | $a_{i-1}$ | $d_i$       | $\theta_i$      |
|-----|-----------------|-----------|-------------|-----------------|
| 1   | 0               | 0         | 0           | $\theta_1$      |
| 2   | 0               | 0         | $a_1 + d_2$ | $\frac{\pi}{2}$ |
| 3   | $\frac{\pi}{2}$ | $a_2$     | $d_3 + a_3$ | 0               |

Plugging into Equation 3.6, or the mathematica function gives the forward kinematics

$${}^0_3T = \begin{bmatrix} -\sin \theta_1 & 0 & \cos \theta_1 & (d_3 + a_3) \cos \theta_1 - a_2 \sin \theta_1 \\ \cos \theta_1 & 0 & \sin \theta_1 & a_2 \cos \theta_1 + (d_3 + a_3) \sin \theta_1 \\ 0 & 1 & 0 & a_1 + d_2 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

### 3. (Craig, 3.21)

For this problem, take the zero position of the links as follows:

- for link 1, let  $d_1 = 0$  in the middle (where pictured);
- for link 2, let  $d_2 = 0$  when the link is in the middle (to the left of where pictured); and,
- for link 3, let  $d_3 = 0$  when the link is all the way “down.”

Note that I picked joint axis 1 in the middle of the mechanism.

The link frame assignments are illustrated in Figure 3.

Consulting the figure, the following link parameters are apparent:

| $i$ | $\alpha_{i-1}$   | $a_{i-1}$ | $d_i$ | $\theta_i$       |
|-----|------------------|-----------|-------|------------------|
| 1   | 0                | 0         | $d_1$ | 0                |
| 2   | $-\frac{\pi}{2}$ | 0         | $d_2$ | $-\frac{\pi}{2}$ |
| 3   | $-\frac{\pi}{2}$ | 0         | $d_3$ | 0                |

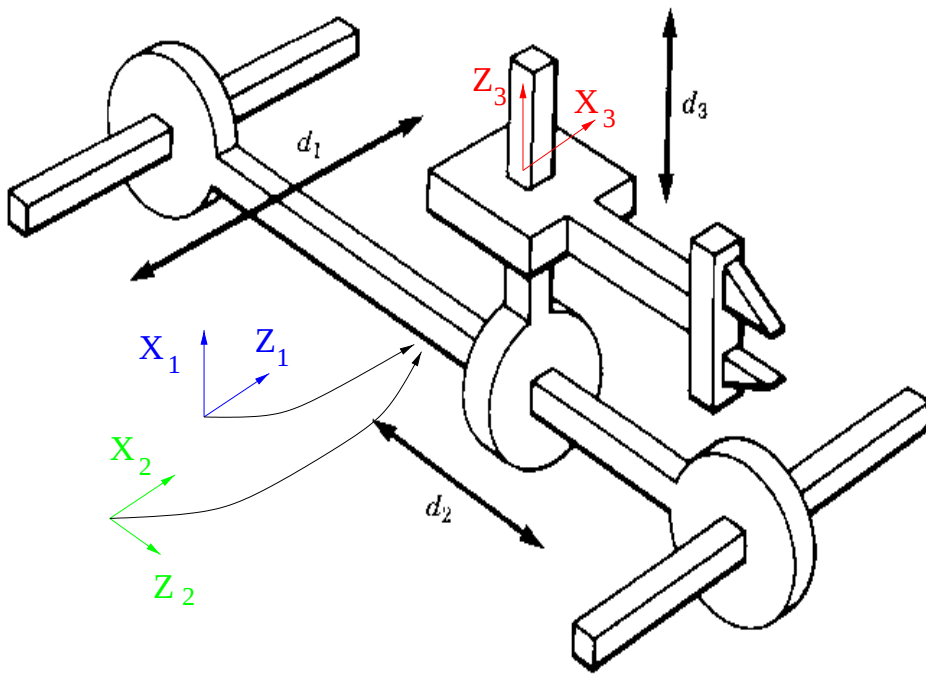
Plugging into Equation 3.6, or the Mathematica function gives the forward kinematics

$${}^0_3T = \begin{bmatrix} 0 & 0 & 1 & d_3 \\ 0 & -1 & 0 & d_2 \\ 1 & 0 & 0 & d_1 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

### 4. (Craig, 5.12)

This problem could be done intuitively:

- Workspace boundary singularity: at  $\theta_2 = \theta_3 = 0$ .
- Interior singularity: at  $\theta_2 = \pi$ .



**Figure 3.** Link frame assignments for problem 3.

5. (Craig, 5.18)

This is just asking for the linear part, so all we have to do is differentiate the top three terms of the fourth column:

$${}^0P_{3ORG} = \begin{bmatrix} l_1 c_1 + l_2 c_1 c_2 \\ l_1 s_1 + l_2 s_1 c_2 \\ l_2 s_2 \end{bmatrix},$$

therefore

$${}^0\dot{P}_{3ORG} = \begin{bmatrix} -\dot{\theta}_1(l_1 s_1 + l_2 s_1 c_2) - \dot{\theta}_2 l_2 c_1 s_2 \\ \dot{\theta}_1(l_1 c_1 + l_2 c_1 c_2) - \dot{\theta}_2 l_2 s_1 s_2 \\ \dot{\theta}_2 l_2 c_2 \end{bmatrix},$$

or, in matrix form,

$${}^0J(\Theta) = \begin{bmatrix} -l_1 s_1 - l_2 s_1 c_2 & -l_2 c_1 s_2 & 0 \\ l_1 c_1 + l_2 c_1 c_2 & -l_2 s_1 s_2 & 0 \\ 0 & l_2 c_2 & 0 \end{bmatrix}.$$

6. (Craig, 5.19)

Using the general definition of a Jacobian directly gives:

$$J(\Theta) = \begin{bmatrix} -a_1 s_1 - d_2 c_1 & -s_1 \\ a_1 c_1 - d_2 s_1 & c_1 \end{bmatrix}.$$

Now,

$$\det(J(\Theta)) = -d_2.$$

Therefore, the manipulator is at a singular configuration when

$$d_2 = 0.$$